



# **Non Linear Control of a Distributed Solar Field**

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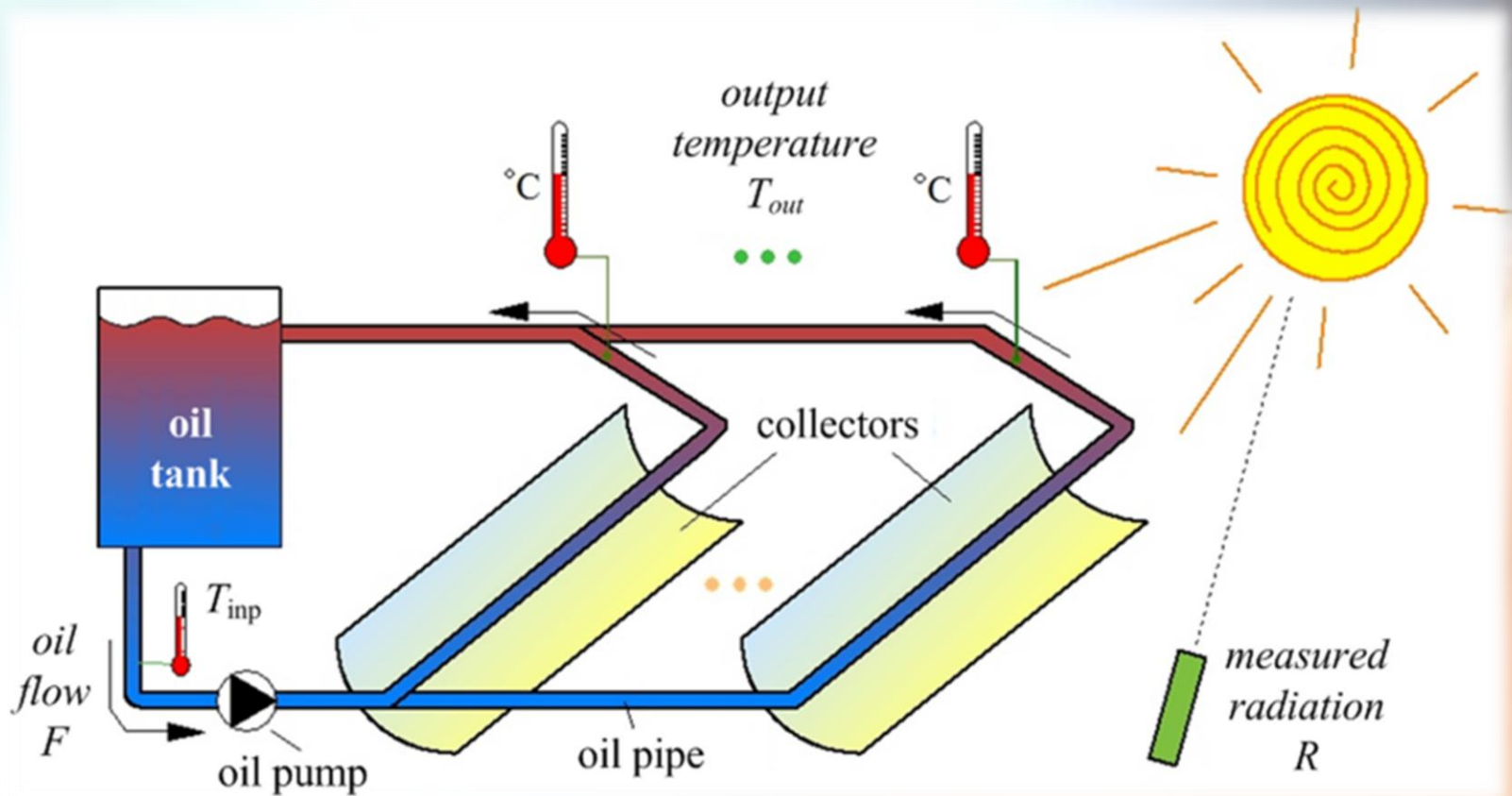
# ACUREX Solar Field



# Parabolic through collector



# Solar plant scheme

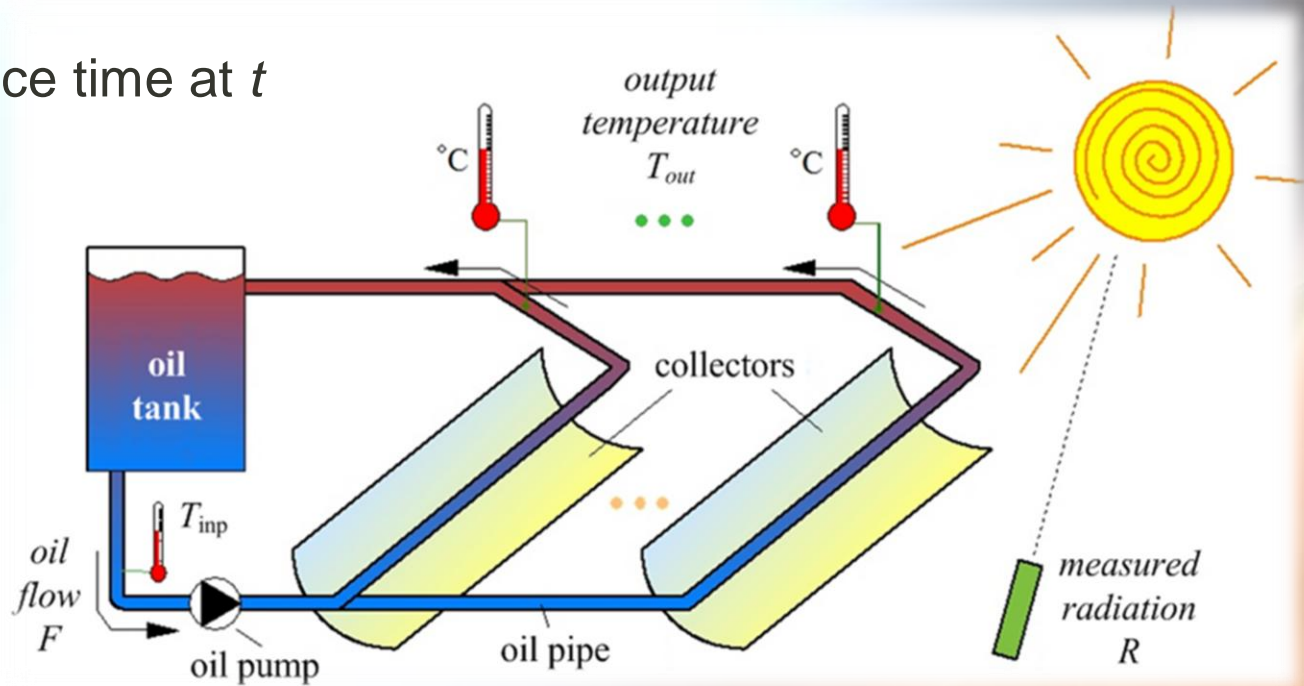


The action on the **pump's flow** changes the residence time of the oil inside the active part of the field, changing the **output temperature**.

The **solar radiation** and **input temperature** are plant **disturbances**.

# Plant model (integral version)

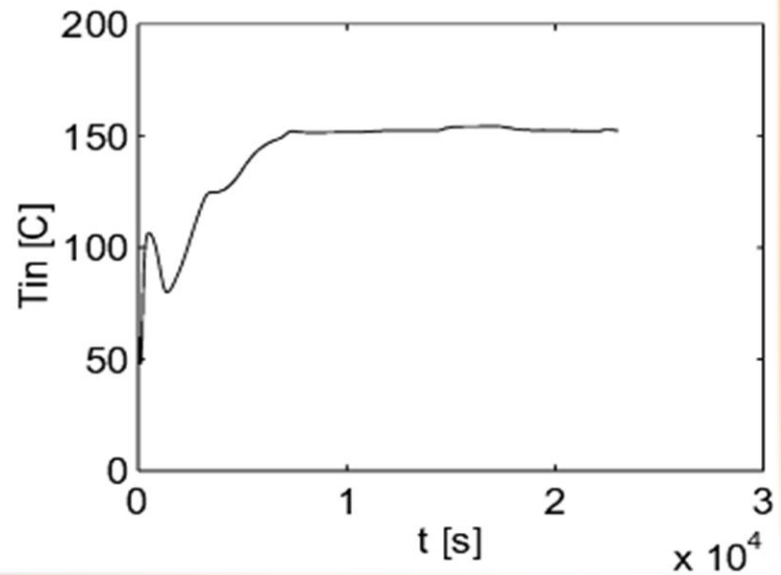
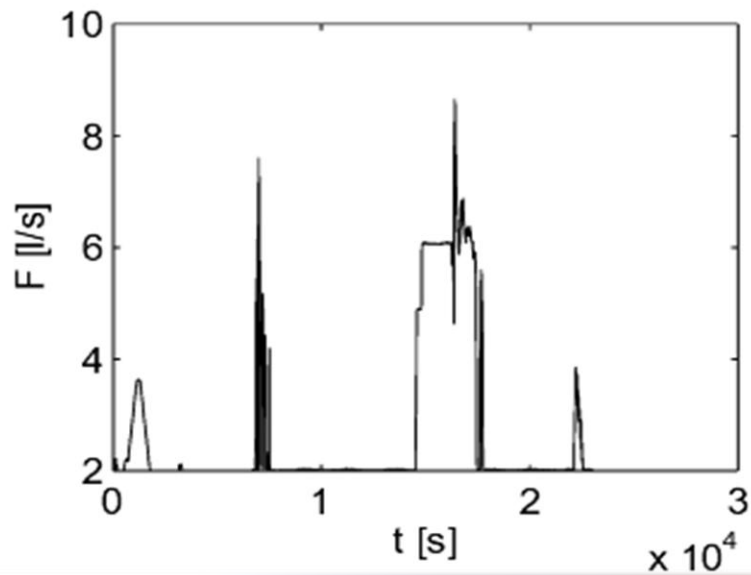
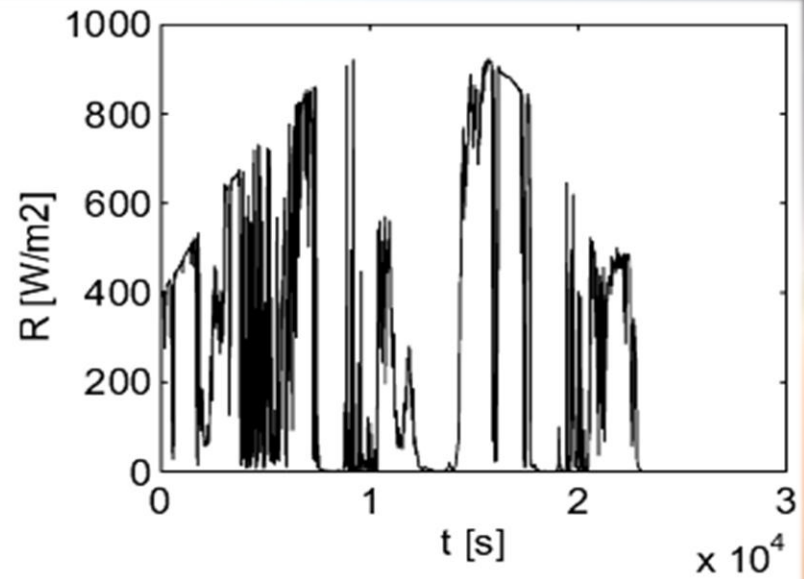
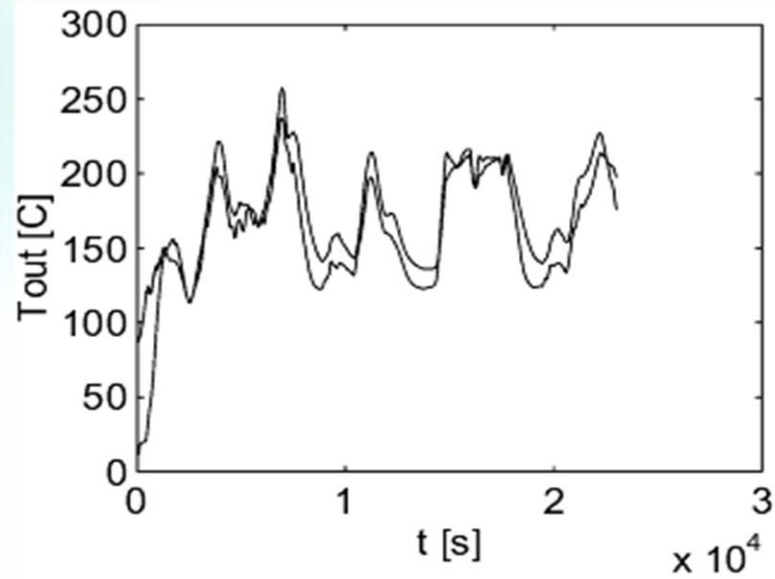
$\tau(t)$  – residence time at  $t$



$$T_{\text{out}}(t) = T_{\text{inp}}(t - \tau(t)) + \alpha \cdot \int_{t - \tau(t)}^t R(\sigma) d\sigma$$

$$\int_{t - \tau(t)}^t F(\sigma) d\sigma = V \quad = \text{active pipe's volume}$$

# Model validation



# Steady-state analysis

If  $R$  is constant, there is a **steady state solution** as:

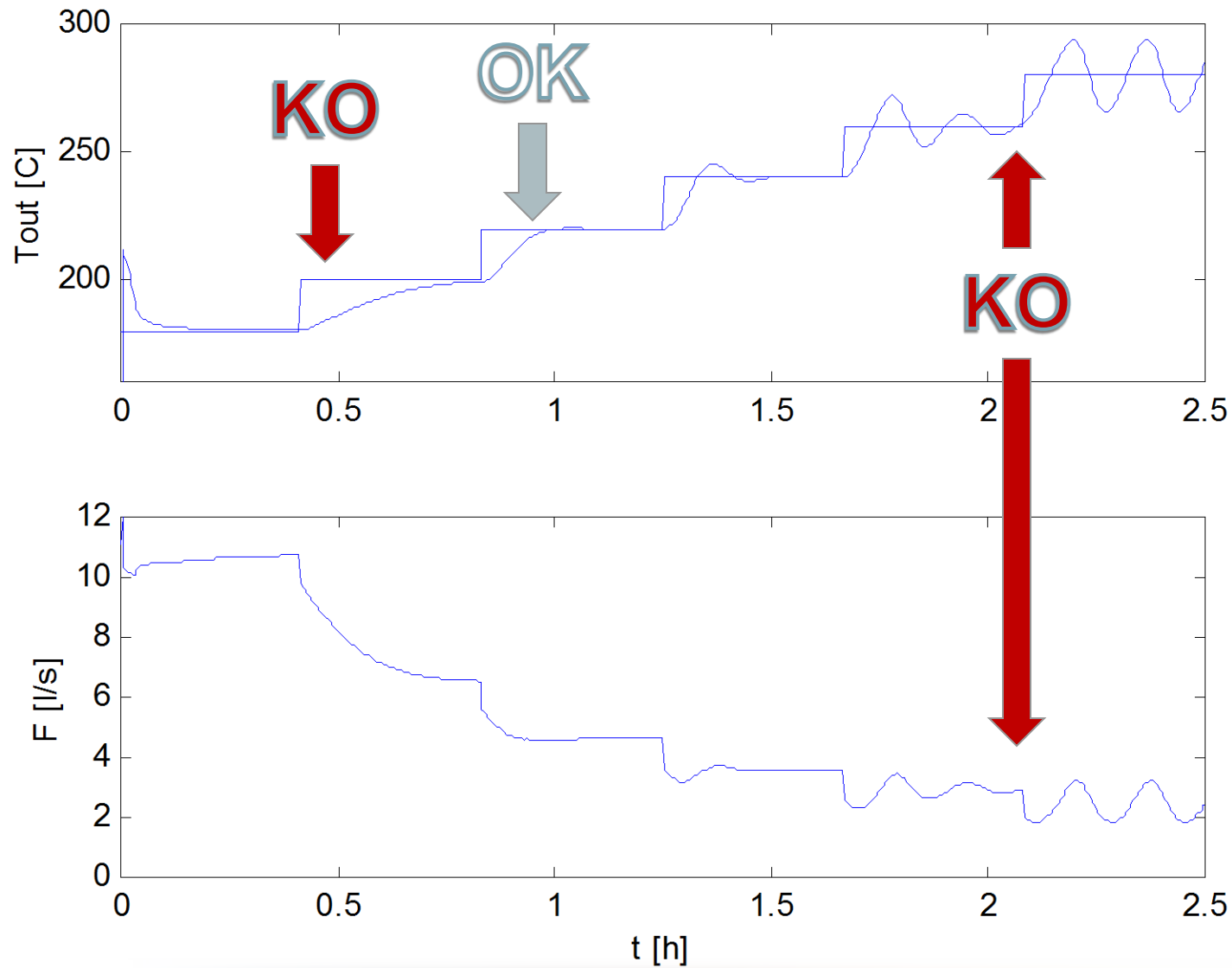
$$\int_{t-\tau(t)}^t F(\sigma) d\sigma = V \quad \longrightarrow \quad \bar{F} \cdot \bar{\tau} = V$$

$$T_{\text{out}}(t) - T_{\text{inp}}(t - \tau) = \alpha \cdot \int_{t-\tau}^t R(\sigma) d\sigma$$



$$\bar{T}_{\text{out}} - \bar{T}_{\text{inp}} = \alpha \cdot \bar{R} \cdot \bar{\tau} = \alpha \cdot \bar{R} \cdot \frac{V}{\bar{F}}$$

# PID Controller...

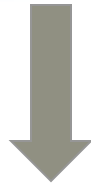




# Proposed solution

From the **steady state solution**:

$$\bar{T}_{\text{out}} - \bar{T}_{\text{inp}} = (\alpha \cdot V) \cdot \frac{\bar{R}}{\bar{F}} \quad \& \quad \bar{\tau} = \frac{V}{\bar{F}}$$



Make PID's  
**proportional gain  $K_P$**   
proportional to

$$\times \frac{F}{R}$$

**gain inversion**

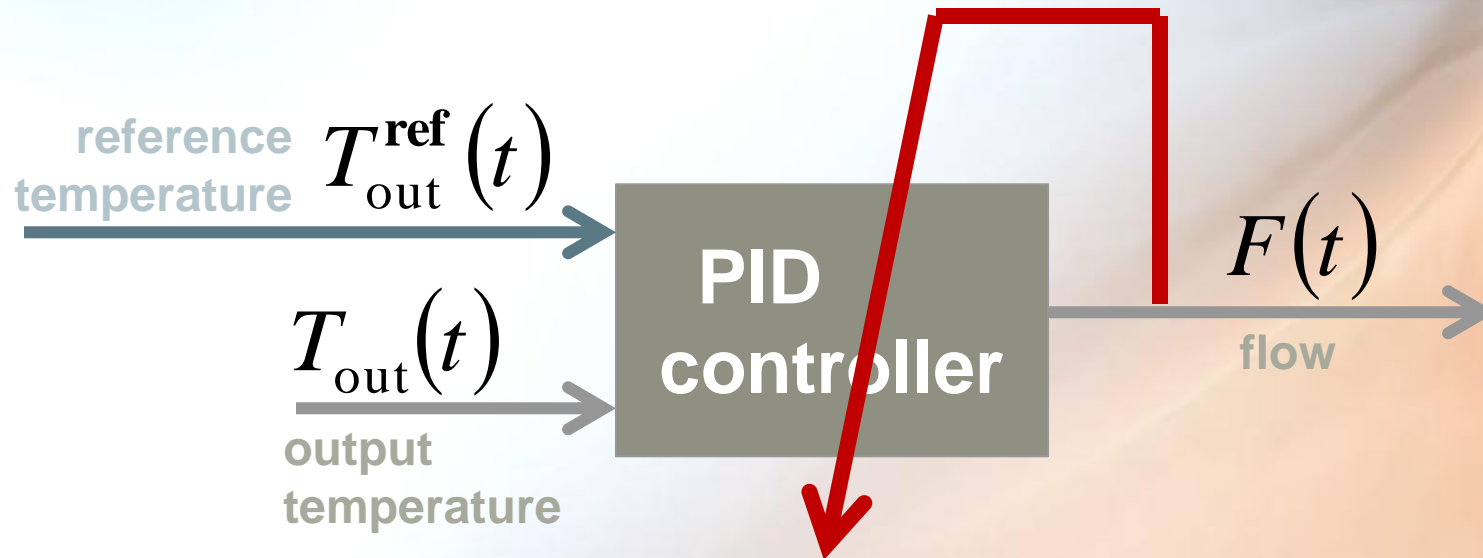
Make PID's  
**integral and derivative times,  $T_I$  and  $T_D$** , proportional to

$$\times \frac{1}{F}$$

**time compliance**

# But we have a problem...

We are doing **gain scheduling** using as **scheduling variable** the resulting control action:



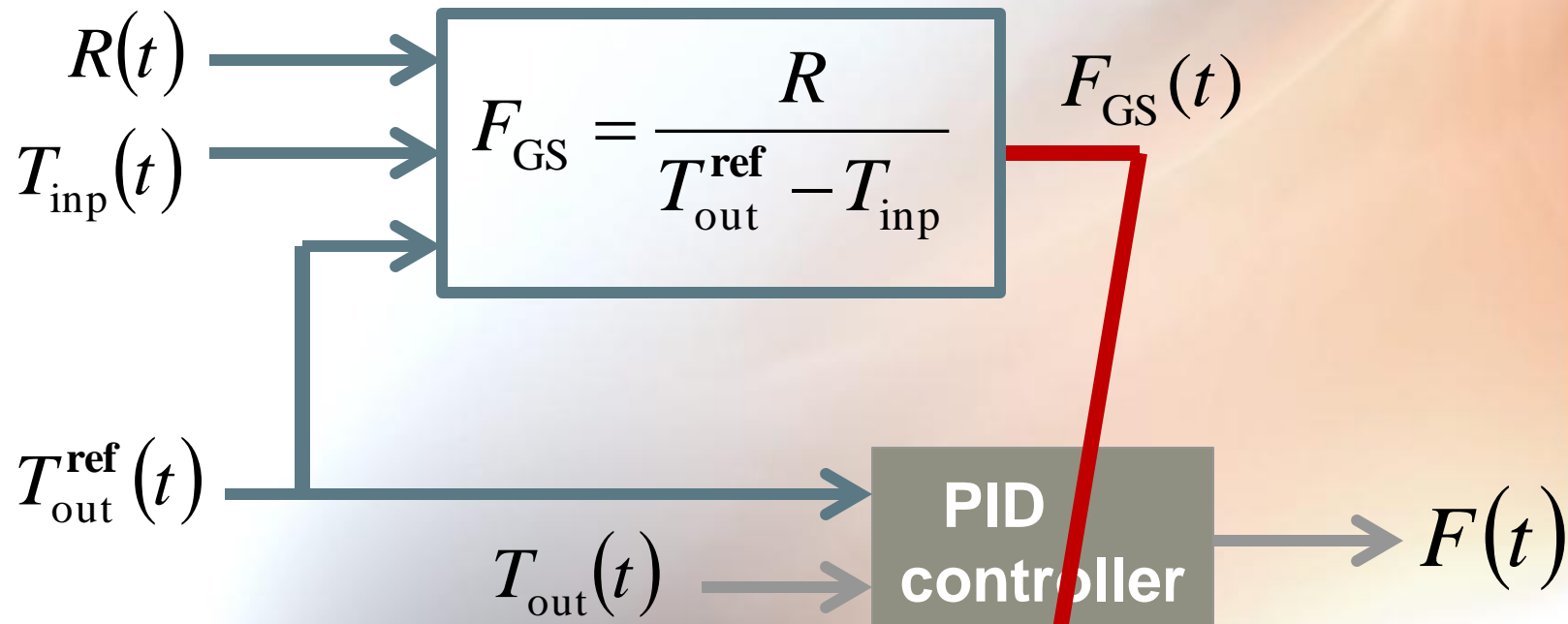
from GS literature: **potential stability problems!**

# ... and the solution:

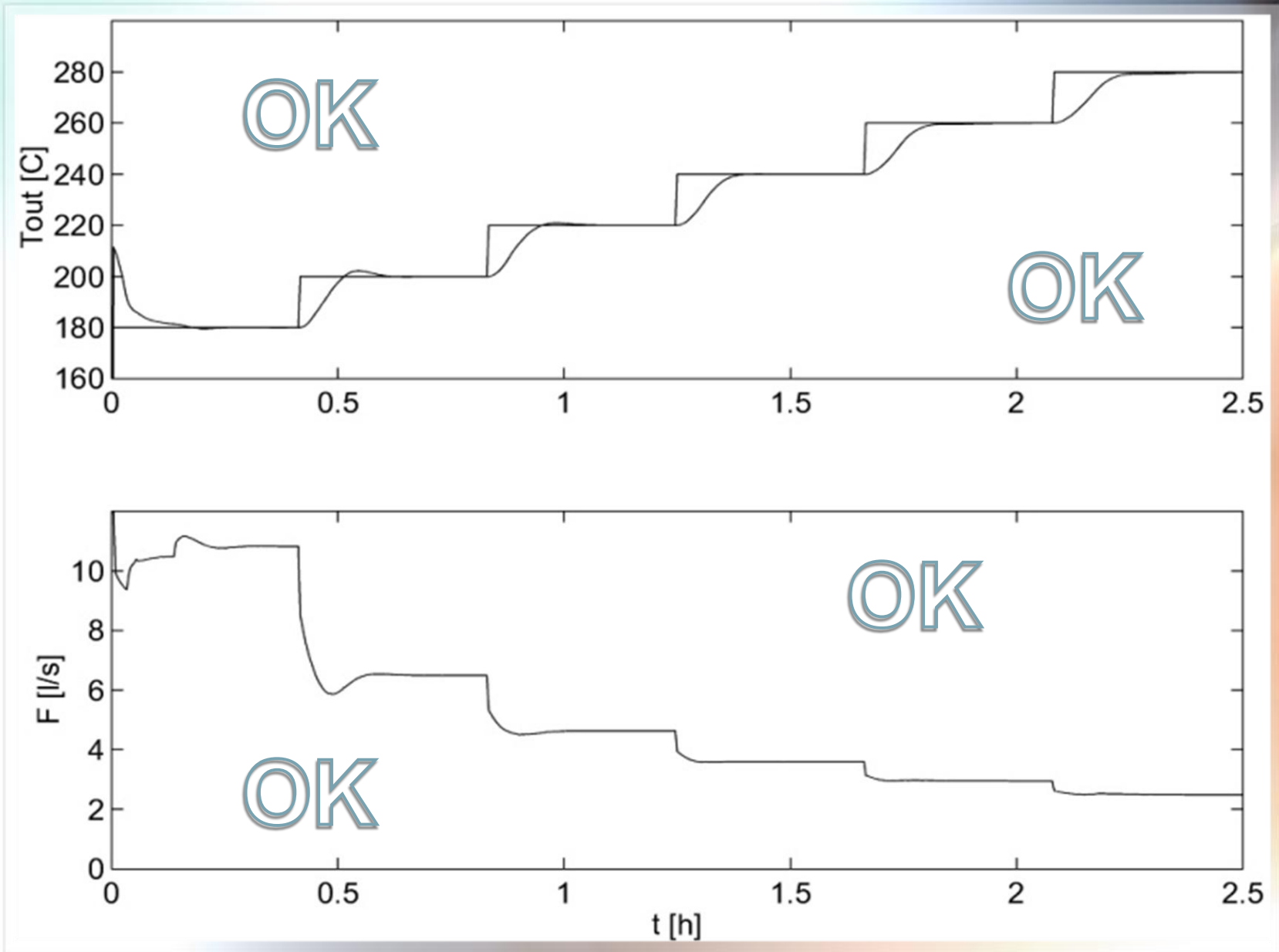
Use again the **steady-state** relationship

$$\bar{T}_{\text{out}} - \bar{T}_{\text{inp}} = (\alpha \cdot V) \cdot \frac{\bar{R}}{\bar{F}}$$

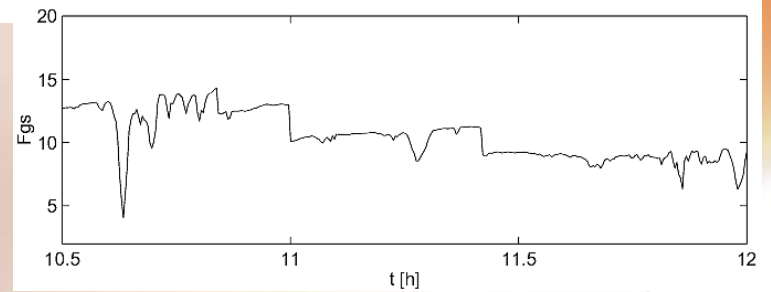
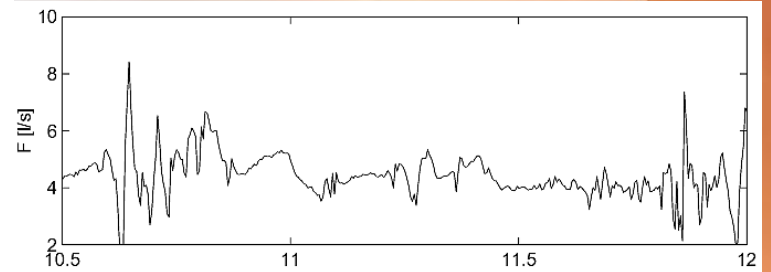
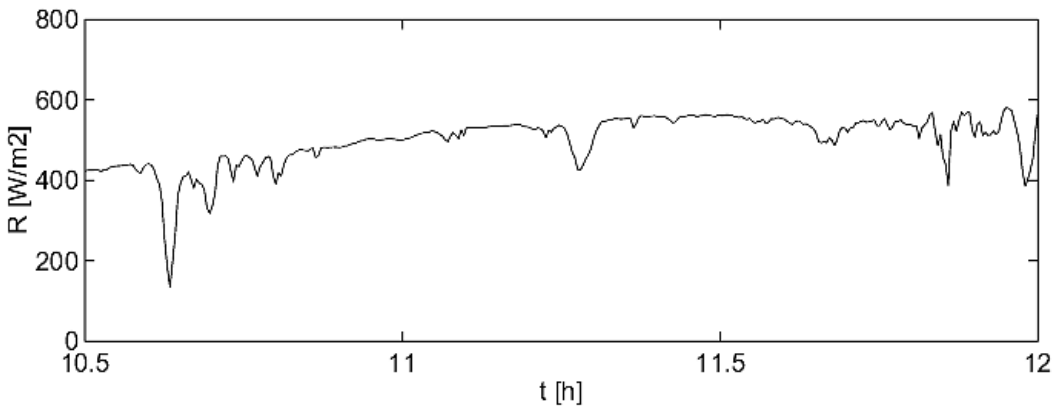
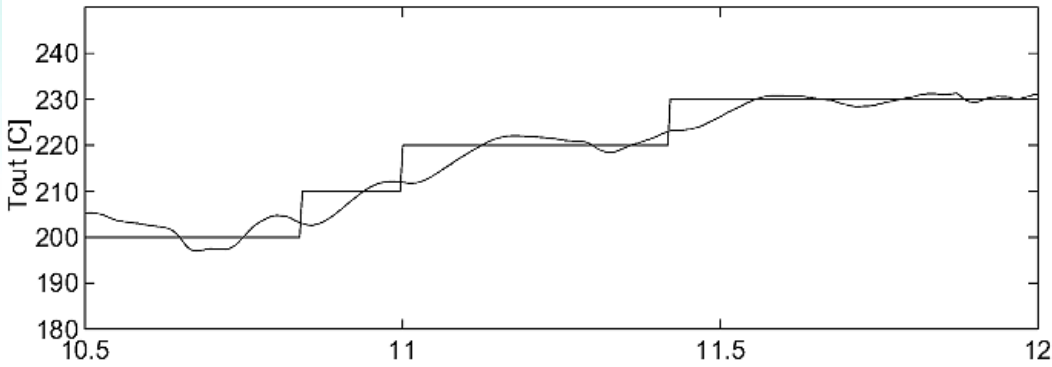
to define a **virtual steady-state flow** to be used as scheduling variable as



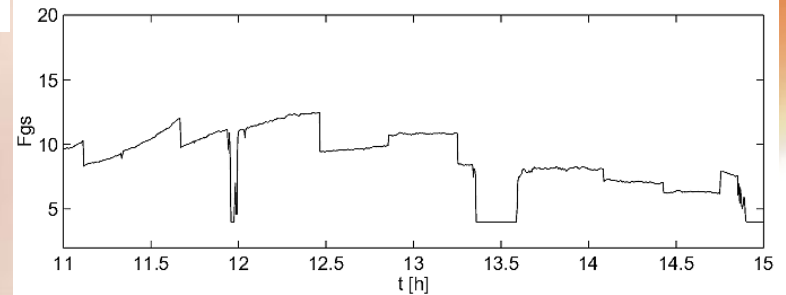
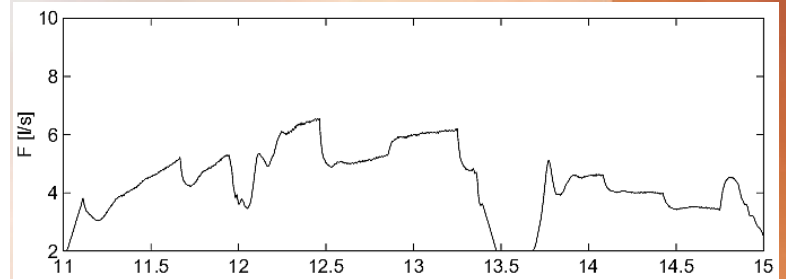
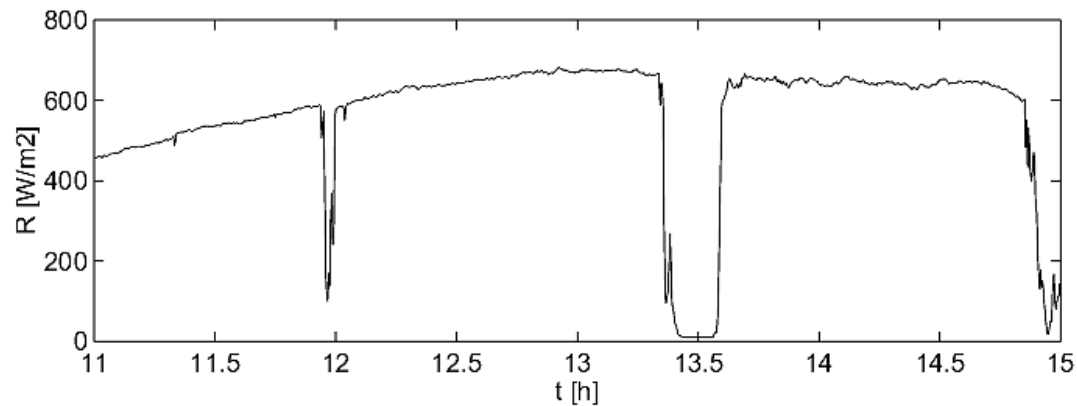
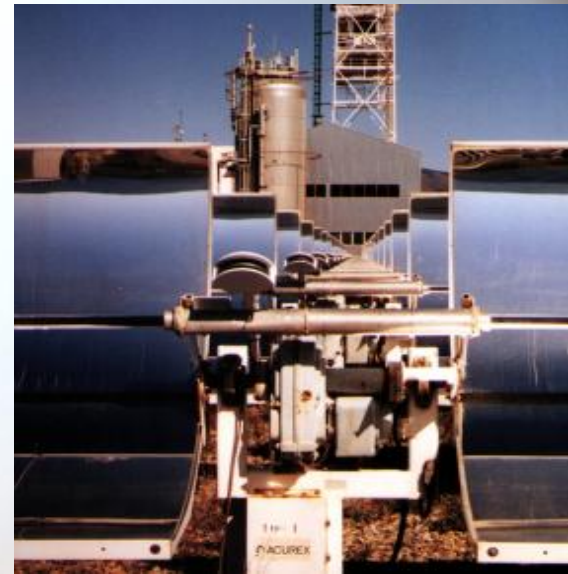
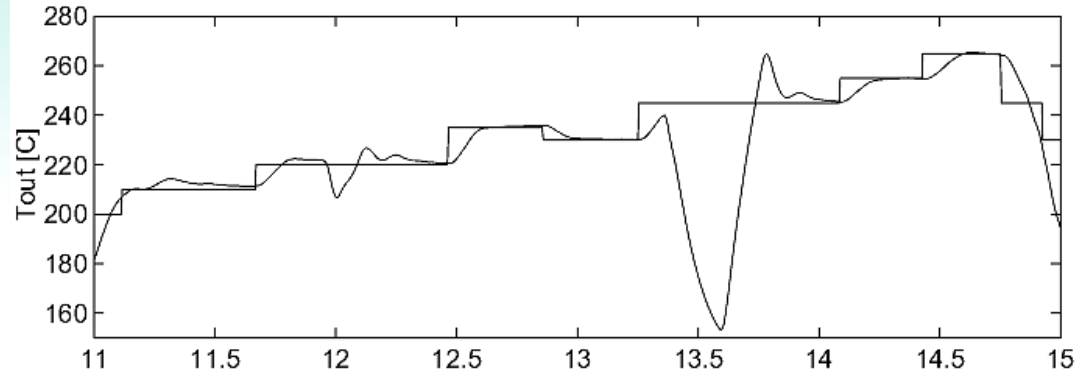
# Simulation results



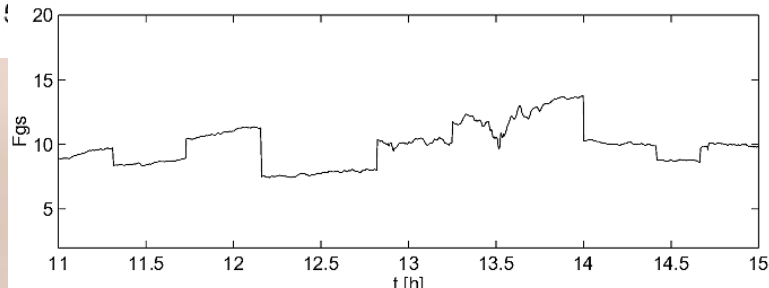
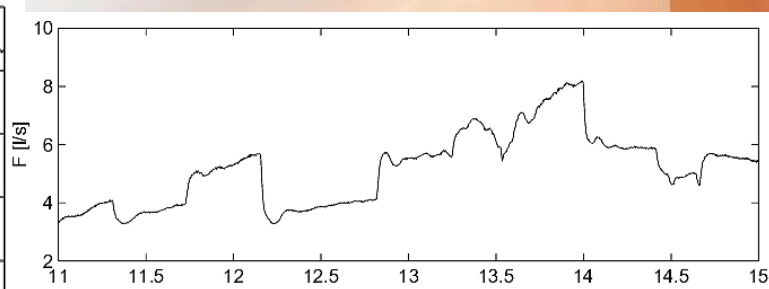
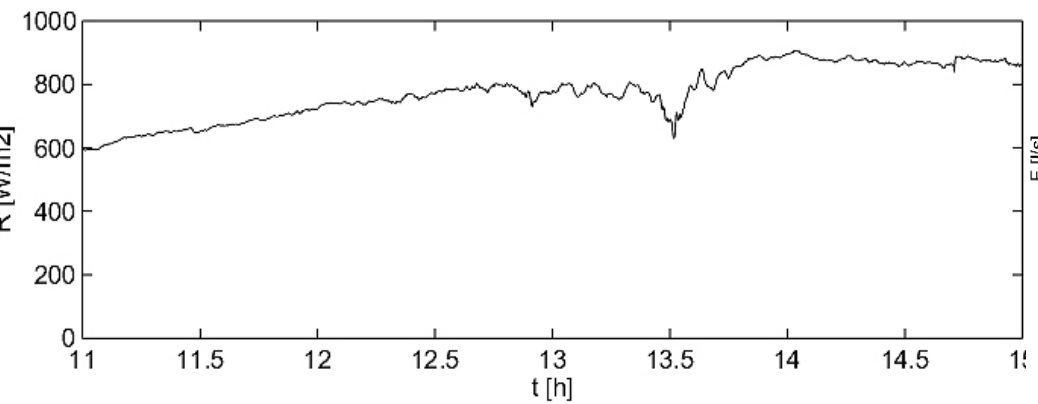
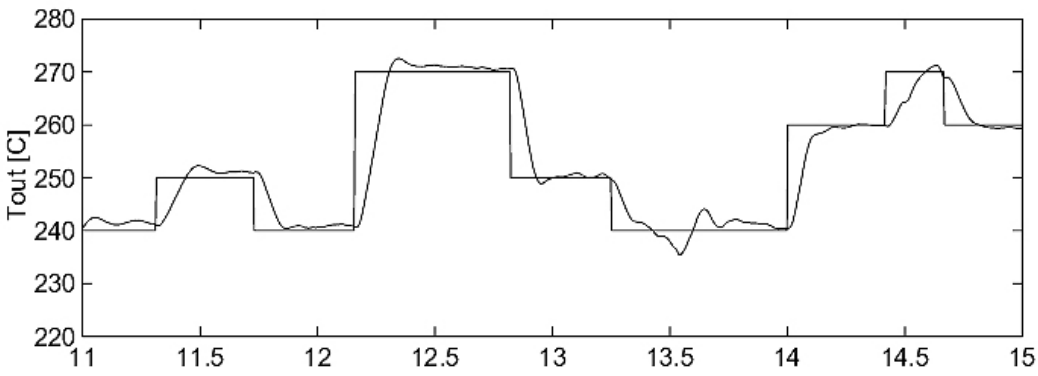
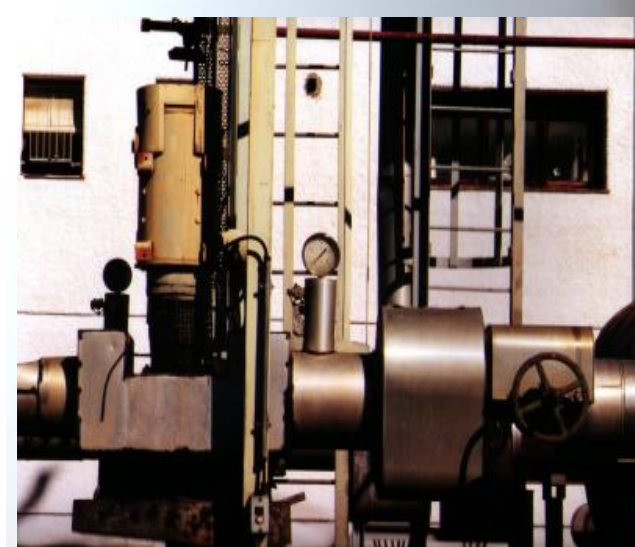
# Experimental results I



# Experimental results II



# Experimental results III



# Conclusions

- Parabolic through collector fields exhibit non-linear dynamic behavior, mainly due to the flow variation;
- **Fixed gain PID controllers do not give satisfactory performance for all operating range;**
- A solution based on the steady-state relationship between radiation, flow and temperatures is presented;
- **The controller gain inverts the plant's dependency on flow; and the controller times are made compliant with the residence time;**
- A virtual flow is computed from external signals to be used as scheduling variable, avoiding an additional feedback loop;
- **Experimental results at the ACUREX field provide favorable evidence on the approach's performance.**





**...the investment  
continues!**

**Thank you!**

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# Some additional references

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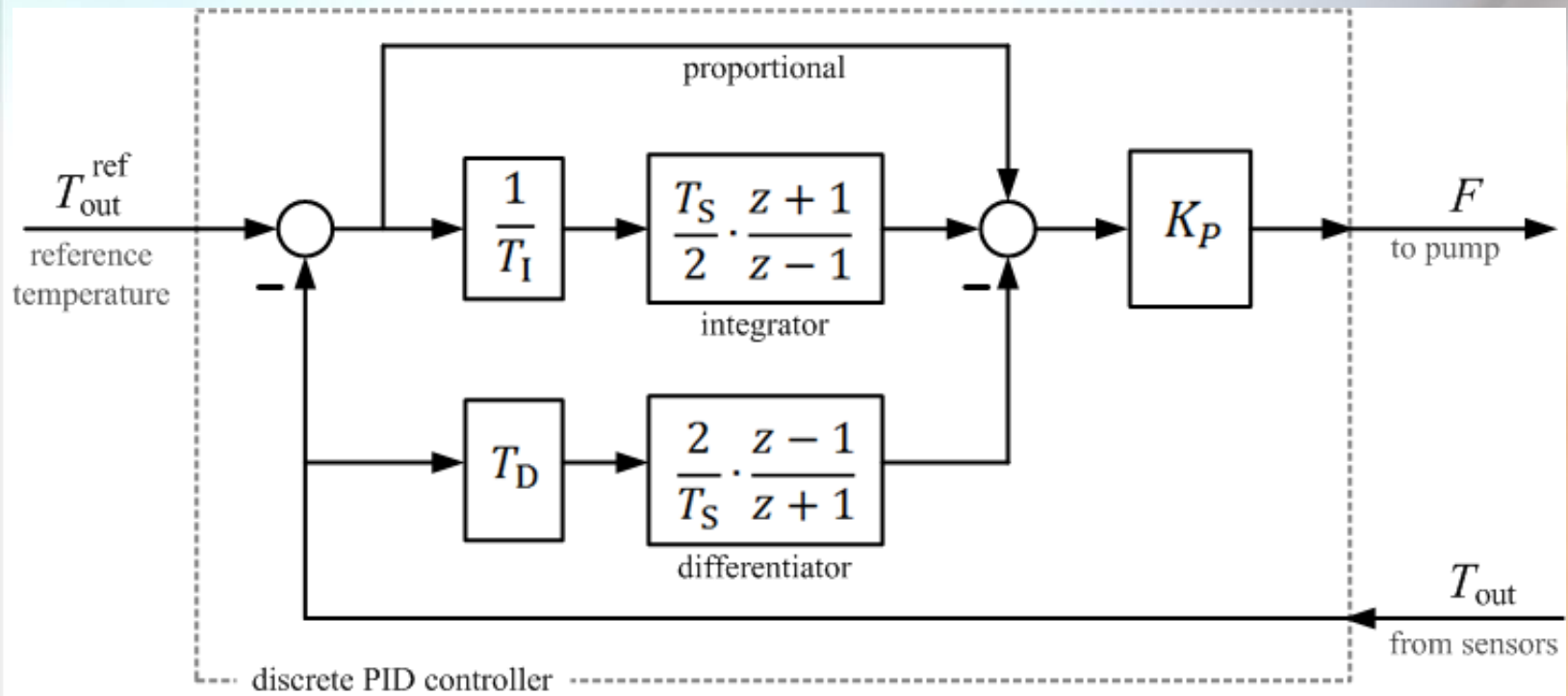
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# Q&A: PID controller



# Q&A: Gain scheduling PID

